

5.2 - Linear Models: Boundary-Value Problems

Consider $y'' + 3y = 0$, $y(0) = 0$, $y(\pi) = 0$

boundary conditions

This has the trivial solution $y = 0$.

We can find that $y = a \cos(\sqrt{3}x) + b \sin(\sqrt{3}x)$

Since $y(0) = 0$, $a = 0$

$$y(\pi) = 0 \Rightarrow b \sin(\sqrt{3}\pi) = 0 \Rightarrow b = 0$$

We only have the trivial solution.

Now consider $y'' + 4y = 0$, $y(0) = 0$, $y(\pi) = 0$

$$y = a \cos 2x + b \sin 2x \quad \rightarrow \quad a = 0$$

$$y = b \sin 2x \quad \text{with} \quad y(\pi) = 0$$

$$0 = b \sin 2\pi \quad \text{holds true} \quad \forall b \in \mathbb{R}.$$

Then $y = b \sin 2x$ is a solution to the BVP for $b \in \mathbb{R}$. The BVP has an infinite number of solutions.

Definition: A number λ for which there exist nontrivial solutions to

$y'' + P(x)y' + \lambda Q(x)y = 0$, $y(a) = 0$, $y(b) = 0$ is called an **eigenvalue**, and a solution $y = ay_1 + by_2$ that satisfies the BVP is an **eigenfunction** associated with the eigenvalue λ .

In the previous example, $P(x)=0$, $Q(x)=1$
 $\lambda=4$ is the eigenvalue, and $y=b\sin 2x$
is the eigenfunction.

$y''+3y=0$ has no eigenvalue.

We can generalize this:

Example: Determine eigenvalues and eigenfunctions for

$$y'' + \lambda y = 0, \quad y(0) = 0, \quad y(L) = 0 \quad (L > 0).$$

$$m^2 = 0 \Rightarrow m = 0$$

Case I: $\lambda = 0$. Then $y = ax + b$

and the boundary conditions give $a = b = 0$

$y = 0$ the trivial solution - no eigenvalue

Case II: $\lambda < 0$. Now let $\lambda = -\alpha^2$

$$\text{so } y'' - \alpha^2 y = 0 \Rightarrow m^2 - \alpha^2 = 0 \Rightarrow m = \pm \alpha$$

$$y = a e^{\alpha x} + b e^{-\alpha x}$$

$$\text{Recall } \cosh x = \frac{e^x + e^{-x}}{2}, \quad \sinh x = \frac{e^x - e^{-x}}{2}$$

so we can write $y = a \cosh \alpha x + b \sinh \alpha x$

$$y(0) = 0 \Rightarrow a = 0, \quad y(L) = 0 \Rightarrow b = 0$$

Again, only the trivial solution - no eigenvalue.

Case III: $\lambda > 0$, say $\lambda = \alpha^2$

$$y'' + \alpha^2 y = 0 \Rightarrow m = \pm \alpha i$$

$$y = a \cos \alpha x + b \sin \alpha x$$

$$y(0) = 0 \Rightarrow a = 0, \text{ and } y(L) = 0 \text{ yields}$$

$$b \sin \alpha L = 0$$

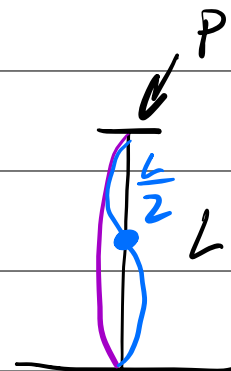
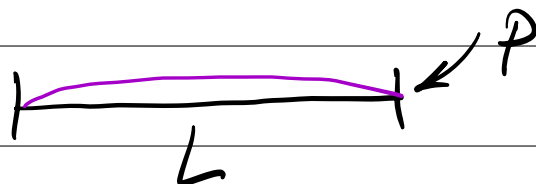
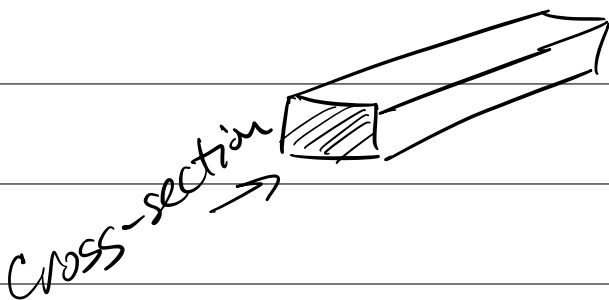
this is zero whenever $\alpha L = n\pi$, $n \in \mathbb{Z}^+$

Assuming $\alpha > 0$ and $L > 0$,

$$\alpha = \frac{n\pi}{L} \Rightarrow \lambda = \alpha^2 = \frac{n^2 \pi^2}{L^2}$$

we have an infinite sequence of eigenvalues:

$$\lambda_n = \frac{n^2 \pi^2}{L^2}, \quad n = 1, 2, 3, \dots$$



Consider a vertical beam of length L with load P applied to one end or a rod with compressive force P applied to one end. Theory of elasticity provides the differential equation $EI \frac{d^2 y}{dx^2} = -Py$ or $EI \frac{d^2 y}{dx^2} + Py = 0$ which in standard form is

$$\frac{d^2 y}{dx^2} + \frac{P}{EI} y = 0$$

The product EI is the flexural rigidity of the beam, E is Young's modulus of elasticity, and I is the moment of inertia of a cross-section of the beam (the shape's inherent resistance to bending).

Considering $P(x) = 0$, $Q(x) = 1$, and letting $\lambda = \frac{P}{EI}$, this has the form

$$y'' + \lambda y = 0$$

With this substitution and considering

$y(0) = 0$, $y(L) = 0$, we have solutions

$$y = b \sin\left(\frac{n\pi x}{L}\right)$$

so the column/rod will buckle/deflect

if $P = \frac{n^2 \pi^2 EI}{L^2}$. When $n=1$, we have

the first buckling load.

If we restrain/support the system

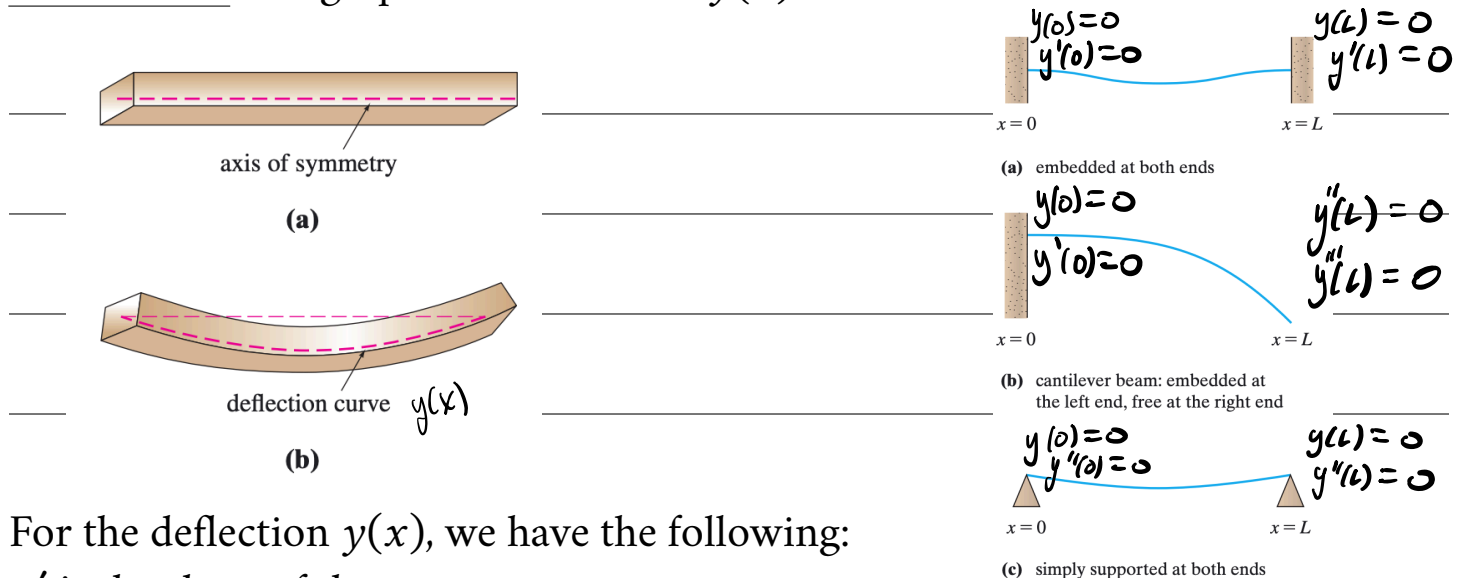
at $\frac{L}{2}$, the smallest critical load

(buckling load) will be $P = \frac{4\pi^2 EI}{L^2}$.

Considering a beam of length L , the bending moment (response or resistance to load) $M(x)$ is related to the load per unit length $w(x)$ by $\frac{d^2 M}{dx^2} = w(x)$ (this is from theory of elasticity). Assuming down is positive, $M(x) = EI\kappa$ is proportional to the curvature of the elastic curve. From multivariable calculus, curvature is $\kappa = \frac{y''}{[1 + (y')^2]^{3/2}}$. For small deflection, $y' = 0$, so $M = EIy''$. We see that $M'' = w(x)$ becomes

$$EI \frac{d^4 y}{dx^4} = w(x)$$

Definition: The graph of the function $y(x)$ is the **deflection curve** of the beam.

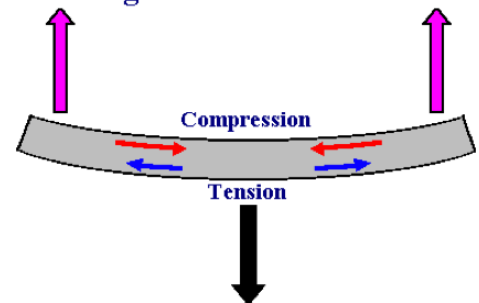


For the deflection $y(x)$, we have the following:

y' is the slope of the curve;
 y'' is the bending moment;
 y''' is the shear force.

If the end of the beam is
embedded, $y = 0$, $y' = 0$
free, $y'' = 0$, $y''' = 0$
simply supported / hinged
 $y = 0$, $y'' = 0$

Compression and Tension in a Bending Beam



Example: Solve the differential equation $EI \frac{d^4 y}{dx^4} = w(x)$ subject to the appropriate boundary conditions. The beam is of length L , and w_0 is a constant.

(a) The beam is simply supported at both ends, and

$w(x) = w_0, 0 < x < L$.

$$\frac{d^4 y}{dx^4} = \frac{w_0}{EI} \Rightarrow y'''' = \frac{w_0}{EI} x + C_1$$

$$y''' = \frac{w_0}{2EI} x^2 + C_1 x + C_2$$

$$y'' = \frac{w_0}{6EI} x^3 + \frac{1}{2} C_1 x^2 + C_2 x + C_3$$

$$y = \frac{w_0}{24EI} x^4 + \frac{1}{6} C_1 x^3 + \frac{1}{2} C_2 x^2 + C_3 x + C_4$$

$$y(0) = y''(0) = y(L) = y''(L) = 0$$

$$\rightarrow C_4 = 0$$

$$\rightarrow C_2 = 0$$

$$y''(L) = 0 \Rightarrow 0 = \frac{w_0}{2EI} L^2 + C_1 L \text{ gives } C_1$$

$$C_1, \text{ with } y(L) = 0 \text{ gives } C_3$$

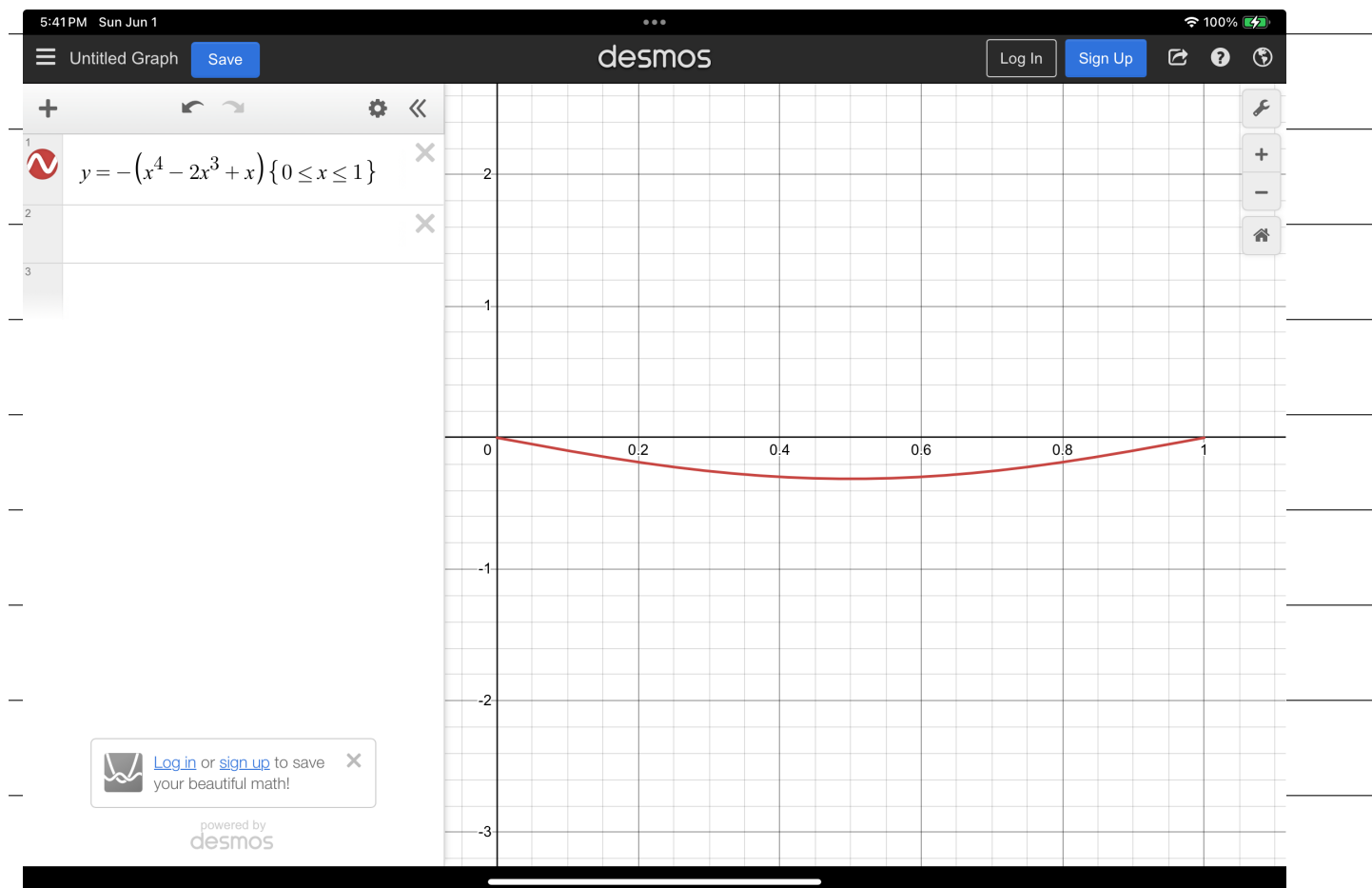
We find that $y(x) = \frac{w_0}{24EI} (x^4 - 2Lx^3 + L^3x)$

(b) Use a graphing utility to graph the deflection curve when

$w_0 = 24EI$ and $L = 1$.

$$y(x) = x^4 - 2x^3 + x, \quad 0 \leq x \leq 1$$

$$\text{Graph } -y(x) = -(x^4 - 2x^3 + x)$$



$$x = \int [(D+1)y - 6] dt + c_3$$

$$Dx + (D+1)y = -6$$

$$4.9: \textcircled{1} (2D+1)(D-1)x - (2D+1)y = 6$$

$$\textcircled{2} (D-1)x + Dy = -6$$

$$\textcircled{1} - (2D+1)\textcircled{2}$$

$$(2D+1)(D-1)x - (2D+1)y = 6$$

$$-(2D+1)(D-1)x - (2D^2+D)y = 6$$

$$(2D^2+3D+1)y = -12$$

$$(2m+1)(m+1) = 0 \Rightarrow m = -\frac{1}{2}, -1$$

$$y_c = c_1 e^{-1/2x} + c_2 e^{-x}, \quad y_p = A \Rightarrow A = -12$$

$$y = c_1 e^{-1/2x} + c_2 e^{-x} - 12$$

$$(2D+1)(D-1)x - (2D+1)y = 6$$

$$(D-1)x + Dy = -6$$

$$D\textcircled{1} + (2D+1)\textcircled{2}$$

$$\overset{D(2D+1)(D-1)x}{(2D^3 - D^2 - D)x} - \cancel{D(2D+1)y} = 0$$

$$\overset{(2D+1)(D-1)x}{(2D^2 - D - 1)x} + \cancel{D(2D+1)y} = -6$$

$$(2D^3 + D^2 - 2D - 1)x = -6$$

$$\underline{2m^3 + m^2 - 2m - 1 = 0}$$

$$(m^2 - 1)(2m + 1) = 0 \Rightarrow m = \pm 1, -\frac{1}{2}$$

$$X_c = c_3 e^t + c_4 e^{-t} + c_5 e^{-1/2 t}$$

$$y_p = A \Rightarrow A = 6$$

$$X(t) = c_3 e^t + c_4 e^{-t} + c_5 e^{-1/2 t} + 6$$

$$y(t) = c_1 e^{-1/2 t} + c_2 e^{-t} - 12$$

$$Dy = -\frac{1}{2} c_1 e^{-1/2 t} - c_2 e^{-t}$$

$$(2D+1)(D-1)X - (2D+1)y = 6$$

$$\underline{(D-1)X} + \underline{Dy} = -6$$

$$Dx = c_3 e^t - c_4 e^{-t} - \frac{1}{2} c_5 e^{-1/2 t}$$

$$\underline{-2c_4 e^{-t} - \frac{3}{2} c_5 e^{-1/2 t} - 6} - \underline{\frac{1}{2} c_1 e^{-1/2 t} - c_2 e^{-t}} = -6$$

$$-2c_4 - c_2 = 0 \quad -\frac{3}{2} c_5 - \frac{1}{2} c_1 = 0$$

$$c_4 = -\frac{1}{2} c_2$$

$$c_5 = -\frac{1}{3} c_1$$

$$X(t) = c_3 e^t - \frac{1}{2} c_2 e^{-t} - \frac{1}{3} c_1 e^{-1/2 t} + 6$$

$$y(t) = c_1 e^{-1/2 t} + c_2 e^{-t} - 12$$

$$\frac{dx}{dt} = -y + t$$

$$Dx + y = t$$

$$\frac{dy}{dt} = x - t$$

$$\rightarrow -D(X - Dy) = t$$

$$(D^2 + 1)y = t - 1 \quad m = \pm i$$

$$y_c = c_1 \cos t + c_2 \sin t, \quad y_p = At + B$$

$$A = 1, B = -1$$

$$y = c_1 \cos t + c_2 \sin t + t - 1 \rightarrow \textcircled{1} \quad Dx = -y + t$$

$$Dx = \int (-c_1 \cos t - c_2 \sin t + 1) dt$$

$$x = -c_1 \sin t + c_2 \cos t + t + c_3 \quad \checkmark$$

$$x - Dy = t : \quad -c_1 \sin t + c_2 \cos t + t + c_3 - c_1 \cos t - c_2 \sin t - 1 = t$$

$$c_3 = 1$$

$$x = -c_1 \sin t + c_2 \cos t + t + 1$$

$$y = c_1 \cos t + c_2 \sin t + t - 1$$